The prestressing effect was applied through an initial strain, an option offered by this element. As a result of an initial parametric investigation, it was found that the maximum initial strain numerically possible was 0.0045 in/in, instead of the 0.0052 in/in considered by Hassan and Rizkalla (2004).

For the behavior of the concrete elements, the material characteristics predefined in the "Concrete Non-Metal Plasticity" model were used to generate a multilinear isotropic model (MISO). The MISO curve was generated as is presented in Kachlakev et al. (2001). The modulus of elasticity E and the tensile strength f_r were derived from the nominal value of the ultimate compressive strength f_c . During the analysis, same convergence problem was faced due to low shear transfer coefficient β_t . After a few preliminary analyses, a 0.25 value was considered to be used in further investigations. This value is similar to other researchers' findings. See Table 3.1 for a comparison of the material characteristics for the two concrete structural members used in the analyses. For the reinforcements (GFRP and prestressing tendons), a perfectly elasto-plastic bilinear isotropic (BISO) model was considered, as presented in Table 3.2.

Table 3.1 Concrete Properties

| Material property | Deck | Girder |
|---|-------|--------|
| Modulus of elasticity E [ksi] | 3,370 | 4,030 |
| Compressive strength f' _c [psi] | 3,500 | 5,000 |
| Tensile (rupture) strength f _r [psi] | 444 | 530 |
| Shear transfer coefficient β_t | 0.25 | 0.25 |
| Poisson's ratio v | 0.2 | 0.2 |

Table 3.2. Reinforcing Material Properties

| Material Property | Smeared GFRP | Steel Prestressing |
|--|--------------|--------------------|
| | rods | tendons |
| Modulus of elasticity E [ksi] | 5900 | 29000 |
| Ultimate tensile strength F _u [ksi] | 72 | 270 |
| Poisson's ratio v | 0.3 | 0.3 |